

Optimal Voltage Control of Non-Stationary Eddy Current Problems

December 4, 2017

FREDI TRÖLTZSCH

Institut für Mathematik
Technische Universität Berlin
D-10623 Berlin, Germany

ALBERTO VALLI ¹

Dipartimento di Matematica
Università di Trento
38123 Trento, Italy

Abstract

A mathematical model is set up that can be useful for controlled voltage excitation in time-dependent electromagnetism. The well-posedness of the model is proved and an associated optimal control problem is investigated. Here, the control function is a transient voltage and the aim of the control is the best approximation of desired electric and magnetic fields in suitable L^2 -norms. Special emphasis is laid on an adjoint calculus for first-order necessary optimality conditions. Moreover, a peculiar attention is devoted to propose a formulation for which the computational complexity of the finite element solution method is substantially reduced.

Dedicated to Prof. Dr. Eduardo Casas on the occasion of his 60th birthday

¹The first author was supported by Einstein Center for Mathematics Berlin (ECMath), project D-SE9. The second author is pleased to thank the Institute of Mathematics of the Technische Universität Berlin, the Research Center Matheon and the Einstein Center for Mathematics Berlin (ECMath) for their kind hospitality.

1 Introduction

In the last two decades, the optimal control of electromagnetic fields received increasing attention. Optimal control problems for processes in magnetohydrodynamics (MHD) were studied extensively since the mid of the 90ies. We mention exemplarily [15, 16, 13, 14, 11, 23, 10, 12, 9] and the references therein. Here, the state equations account for the flow of electrically conducting fluids and for the electromagnetic field. In the last years, the numerical analysis of controlled electric or magnetic fields in electrically conducting media became more active. We mention, for instance, [4, 26, 20, 21, 27, 22, 6]. In the majority of these papers, distributed and/or time-dependent electrical currents were considered as controls.

The control of electrical voltages was first investigated in the time-harmonic case, see [17, 18, 28, 24, 25]. Here, the dynamical system is of elliptic type. Often, it is more realistic to control the electrical voltage in a non-harmonic setting. This leads to specific issues of modeling and mathematical analysis. To our best knowledge, only the papers [28, 20, 21] considered the optimal control of electromagnetic fields by the electrical voltage. A vector potential ansatz was applied to convert the standard magneto-quasistatic Maxwell equations in a (degenerate) parabolic system.

In our paper, the mathematical analysis for the optimal control of voltages is the central aspect. The associated model for the electromagnetic fields is close to that proposed in the seminal paper [5]. We follow a slightly different approach. We merge the modeling ideas of [5] with both a specific approach aiming at reducing the complexity of the Maxwell equations for given voltages and some ideas of adjoining in [24, 25]. We should notice that, using our approach, specific difficulties arise in the process of adjoining. Here, differential operators on the boundary, namely, the surface gradient and the surface divergence, can be invoked to overcome this obstacle. The paper is organized as follows: in Section 2 we point out some assumptions and deduce the eddy current model. In Section 3 we devise the weak formulation of the problem and prove that it is well-posed. In Section 4 we derive the strong formulation, which shows more explicitly the role of the equations and boundary conditions, and that can be the starting point for non-variational numerical approximation methods. The fifth section is devoted to the formulation of the optimal control problem, whereas in Section 6 the adjoint problem and the necessary optimality conditions

are derived. Some remarks on numerical approximation are included in Section 7.

2 Modeling the Maxwell system

The non-stationary Maxwell system reads

$$\begin{aligned}
 \frac{\partial \mathbf{B}}{\partial t} + \operatorname{curl} \mathbf{E} &= \mathbf{0} \\
 \frac{\partial \mathbf{D}}{\partial t} + \mathbf{J}_T &= \operatorname{curl} \mathbf{H} \\
 \operatorname{div} \mathbf{B} &= 0 \\
 \operatorname{div} \mathbf{D} &= \rho,
 \end{aligned} \tag{2.1}$$

where \mathbf{B} , \mathbf{H} , \mathbf{D} , and \mathbf{E} denote the magnetic induction, the magnetic field, the electric induction, and the electric field, respectively, and the following constitutive relations hold: $\mathbf{D} = \varepsilon \mathbf{E}$, $\mathbf{B} = \mu \mathbf{H}$, $\mathbf{J}_T = \sigma \mathbf{E} + \mathbf{J}$. The field \mathbf{J} represents the applied electrical current surface density. The coefficients ε and μ are called electrical permittivity and magnetic permeability, respectively: they are symmetric and (uniformly) positive definite matrices, with bounded and measurable real functions as their entries. The same holds in the conducting region for the electrical conductivity σ , which vanishes in non-conducting regions. Also the electric charge volume density ρ is assumed to vanish in non-conducting regions.

Disregarding the displacement current term $\frac{\partial \mathbf{D}}{\partial t}$, we find the eddy current model, in which wave propagation is not taken into account:

$$\begin{aligned}
 \mu \frac{\partial \mathbf{H}}{\partial t} + \operatorname{curl} \mathbf{E} &= \mathbf{0} \quad (\text{Faraday equation}) \\
 \operatorname{curl} \mathbf{H} &= \sigma \mathbf{E} + \mathbf{J} \quad (\text{Ampère equation}) \\
 \operatorname{div}(\mu \mathbf{H}) &= 0 \\
 \operatorname{div}(\varepsilon \mathbf{E}) &= 0.
 \end{aligned} \tag{2.2}$$

Here, the last equation has to be imposed only in non-conducting regions (while the relation $\operatorname{div}(\varepsilon \mathbf{E}) = \rho$ is used for computing the electric charge density in the conducting region, once \mathbf{E} is there available). The electrical voltage is not directly visible in the Maxwell equations.

Therefore, it is most natural that in control problems the electrical current was preferred as considered control.

Controlled voltages were mainly considered in the time-harmonic case (see the references [28, 20, 21], also cited in the Introduction). Here, instead, we are interested in voltage excitation for the non-stationary case. To set up an associated mathematical model is not a trivial task. We follow the presentation given in [3, Chap. 8] for the time-harmonic case, but we also rely on [5], where the main ideas are presented for including the voltage in the model. The principal novelty of our paper is a complete analysis of a mathematical model that can be used in the context of controlled electrical voltages, in a quite general geometrical setting and also including a numerical approximation scheme based on finite elements. After having established a suitable control model, the associated control theory is more or less standard. Nevertheless, some special tricks are needed to set up an adjoint calculus. Here, we follow ideas of our former papers [24, 25]. Moreover, we slightly modify the model proposed in [5] with a technique, introduced in [1, 2], which reduces the computational complexity of the numerical approximation scheme and can be efficiently applied in any geometrical situation.

Assumption 2.1 (Assumptions on the geometry). The computational domain is a simply-connected bounded open set $\Omega \subset \mathbb{R}^3$, with a connected and Lipschitz boundary $\partial\Omega$. It is split into two Lipschitz subdomains, a conducting region Ω_C and a non-conducting region $\Omega_I = \Omega \setminus \overline{\Omega_C}$; the latter is assumed to be connected. The conducting region Ω_C is not strictly contained in Ω , i.e., $\partial\Omega_C \cap \partial\Omega \neq \emptyset$; the intersection is also assumed to be transversal, namely, the surfaces $\Gamma_C = \partial\Omega_C \cap \partial\Omega$ and $\Gamma = \partial\Omega_C \cap \partial\Omega_I$ intersect transversally. For the sake of simplicity, we suppose that Ω_C is simply-connected. Moreover, we suppose that $\Gamma_C = \Gamma_E \cup \Gamma_J$, where Γ_E and Γ_J are two disjoint and connected surfaces on Γ_C ('electric ports').

In Section 4.1 we present and analyze some more complex geometrical settings for the conducting domain Ω_C .

We set also $\Gamma_I = \partial\Omega_I \cap \partial\Omega$. Therefore, with these notations we have $\partial\Omega_C = \Gamma_E \cup \Gamma_J \cup \Gamma$, $\partial\Omega_I = \Gamma_I \cup \Gamma$ (see Figure 1). The unit outward normal vector on $\partial\Omega$, $\partial\Omega_C$ and $\partial\Omega_I$ will be denoted by \mathbf{n} , \mathbf{n}_C and \mathbf{n}_I , respectively.

We want to model the electromagnetic problem in the case of an

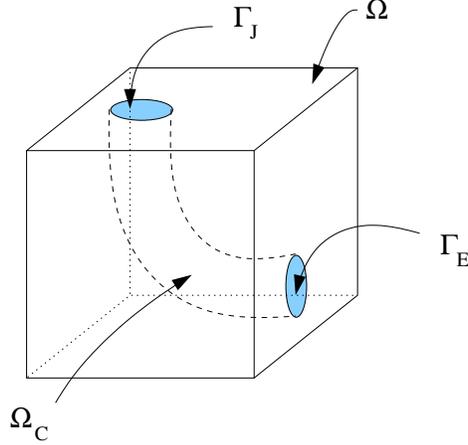


Figure 1: The computational domain Ω with the conductor Ω_C and the electric ports Γ_E and Γ_J .

electric current passing along the ‘cylinder’ Ω_C , and to drive the problem by assigning a potential difference between Γ_E and Γ_J .

Assumption 2.2 (Assumptions on the given data). The matrix-valued functions $\varepsilon \in L^\infty(\Omega_I, \mathbb{R}^{3 \times 3})$, $\mu \in L^\infty(\Omega, \mathbb{R}^{3 \times 3})$ and $\sigma \in L^\infty(\Omega_C, \mathbb{R})$ are assumed to be symmetric and uniformly positive definite in Ω_I , Ω and Ω_C , respectively. The given electrical current density \mathbf{J} belongs to $L^2(0, T; L^2(\Omega)^3)$ and satisfies the necessary condition $\operatorname{div} \mathbf{J}|_{\Omega_I} = 0$ in $\Omega_I \times (0, T)$.

For the sake of simplicity, in Section 3 we will assume $\mathbf{J}|_{\Omega_I} = \mathbf{0}$. However, we note that the case $\mathbf{J}|_{\Omega_I} \neq \mathbf{0}$ is also meaningful: In the modeling of electromagnetic fields, it is often assumed that coils where the current courses through are not viewed as conductors. As a subset of the non-conducting region, they are simply characterized by the presence of an impressed current inside (one can envisage a coil as a package of insulated thin wires, where the current is known).

In order to show more clearly the subdomain where a field is considered, from now on we will write $\mathbf{E}_C := \mathbf{E}|_{\Omega_C}$, $\mathbf{E}_I := \mathbf{E}|_{\Omega_I}$ and use a similar notation for \mathbf{H} . A first point in the modeling is to require that the electric field is normal to the boundary on the two electric ports, namely, $\mathbf{E}_C \times \mathbf{n}_C = \mathbf{0}$ on $\Gamma_E \cup \Gamma_J$. More precisely, as proposed in [7],

for each $t \in [0, T]$ we consider the no-flux boundary conditions

$$\begin{aligned} \mu \mathbf{H} \cdot \mathbf{n} &= 0 && \text{on } \partial\Omega \\ \mathbf{E}_C \times \mathbf{n}_C &= \mathbf{0} && \text{on } \Gamma_E \cup \Gamma_J \\ \varepsilon_I \mathbf{E}_I \cdot \mathbf{n}_I &= 0 && \text{on } \Gamma_I. \end{aligned} \quad (2.3)$$

We refer also to the comments presented in [3, Chap. 8], which show that other possible boundary conditions are not allowed for this type of problem.

In what follows, we will use the tangential differential operators div_τ , curl_τ and grad_τ (see, e.g., [19, Chap. 3], [3, Chap. A1] for their definitions and properties). In particular, for a function ϕ defined on $\partial\Omega$ the tangential operator curl_τ , as usual in a two-dimensional setting, is the rotation of the tangential gradient, namely, $\text{curl}_\tau \phi = \text{grad}_\tau \phi \times \mathbf{n}$; moreover, for a function v defined in $\overline{\Omega}$ it holds $\mathbf{n} \times \text{grad } v \times \mathbf{n} = \text{grad}_\tau(v|_{\partial\Omega})$.

Since $\mu \mathbf{H} \cdot \mathbf{n} = 0$ on $\partial\Omega$, from the Faraday law one has, for each $t \in [0, T]$,

$$0 = -\frac{\partial(\mu \mathbf{H})}{\partial t}(t) \cdot \mathbf{n} = \text{curl } \mathbf{E}(t) \cdot \mathbf{n} = \text{div}_\tau(\mathbf{E}(t) \times \mathbf{n}) \quad \text{on } \partial\Omega.$$

Here, we used the vector calculus identity

$$\text{curl } \mathbf{w} \cdot \mathbf{n} = \text{div}_\tau(\mathbf{w} \times \mathbf{n}),$$

see (3.10) below.

Because Ω is assumed to be simply-connected, the same holds for the surface $\partial\Omega$. Hence the condition $\text{div}_\tau(\mathbf{E}(t) \times \mathbf{n}) = 0$ assures that the tangential field $\mathbf{E}(t) \times \mathbf{n}$ is the tangential curl of some scalar potential: namely, for each $t \in [0, T]$ there exists a potential $v(t) : \overline{\Omega} \mapsto \mathbb{R}$ such that

$$\mathbf{E}(t) \times \mathbf{n} = -\text{curl}_\tau v|_{\partial\Omega}(t) = -\text{grad } v(t) \times \mathbf{n} \quad (2.4)$$

holds on $\partial\Omega$. Moreover, we have $\mathbf{E}_C(t) \times \mathbf{n}_C = \mathbf{0}$ on $\Gamma_E \cup \Gamma_J$. Therefore, since the tangential derivatives of v are vanishing on $\Gamma_E \cup \Gamma_J$, for each $t \in [0, T]$ the function $v(t)$ must be constant on Γ_E and on Γ_J with respect to the space variable \mathbf{x} .

We have thus proved that, under the assumption that Ω is simply-connected, for the eddy current problem the conditions

$$\begin{aligned} \mu \mathbf{H} \cdot \mathbf{n} &= 0 && \text{on } \partial\Omega \\ \mathbf{E}_C \times \mathbf{n}_C &= \mathbf{0} && \text{on } \Gamma_E \cup \Gamma_J \end{aligned}$$

are equivalent to the conditions

$$\begin{aligned}\mu \mathbf{H} \cdot \mathbf{n} &= 0 && \text{on } \partial\Omega \\ \mathbf{E} \times \mathbf{n} &= -\text{grad } v \times \mathbf{n} && \text{on } \partial\Omega \\ v|_{\Gamma_J} \text{ and } v|_{\Gamma_E} &\text{ do not depend on } \mathbf{x}.\end{aligned}$$

The voltage excitation problem thus reads: given $V_E : [0, T] \mapsto \mathbb{R}$ and $V_J : [0, T] \mapsto \mathbb{R}$, we look for a solution of the eddy current problem (2.2) satisfying for each $t \in [0, T]$ the boundary conditions

$$\begin{aligned}\mu \mathbf{H} \cdot \mathbf{n} &= 0 && \text{on } \partial\Omega \\ \mathbf{E} \times \mathbf{n} &= -\text{grad } v \times \mathbf{n} && \text{on } \partial\Omega \\ v|_{\Gamma_J} \text{ and } v|_{\Gamma_E} &\text{ do not depend on } \mathbf{x} && (2.5) \\ v|_{\Gamma_J} - v|_{\Gamma_E} &= V_J - V_E \\ \varepsilon_I \mathbf{E}_I \cdot \mathbf{n}_I &= 0 && \text{on } \Gamma_I,\end{aligned}$$

along with the initial condition $\mathbf{H}|_{t=0} = \mathbf{H}_0 := \mu^{-1} \mathbf{B}_0$. Here the vector field \mathbf{B}_0 has to satisfy the necessary compatibility conditions $\text{div } \mathbf{B}_0 = 0$ in Ω and $\mathbf{B}_0 \cdot \mathbf{n} = 0$ on $\partial\Omega$, that derive from taking the divergence of the Faraday equation (2.2)₁ and from (2.5)₁.

Remark 1. *It is worth noting that, if conditions (2.5) are satisfied, the quantities V_J and V_E are related by*

$$V_J - V_E = - \int_{\hat{\gamma}} \mathbf{E}_I \cdot \boldsymbol{\tau}, \quad (2.6)$$

where $\hat{\gamma}$ is any curve lying on Γ_I and joining the electric port Γ_E to the electric port Γ_J , and $\boldsymbol{\tau}$ is the unit tangent vector on it.

In fact, from (2.5)₂ we know that $\mathbf{E} \times \mathbf{n} = -\text{grad } v \times \mathbf{n}$ on the boundary $\partial\Omega$, and therefore, if a curve $\hat{\gamma}$ lies on $\partial\Omega$ and connects the points \mathbf{p}_- and \mathbf{p}_+ , we have

$$\int_{\hat{\gamma}} \mathbf{E}_I \cdot \boldsymbol{\tau} = - \int_{\hat{\gamma}} \text{grad } v \cdot \boldsymbol{\tau} = -v(\mathbf{p}_+) + v(\mathbf{p}_-).$$

From (2.5)₃ we know that $v|_{\Gamma_J}$ and $v|_{\Gamma_E}$ are constants. Hence, taking any curve $\hat{\gamma} \subset \Gamma_I \subset \partial\Omega$ joining the electric port Γ_E to the electric port Γ_J , we have $v(\mathbf{p}_-) = v|_{\Gamma_E}$ and $v(\mathbf{p}_+) = v|_{\Gamma_J}$, thus

$$\int_{\hat{\gamma}} \mathbf{E}_I \cdot \boldsymbol{\tau} = -v|_{\Gamma_J} + v|_{\Gamma_E}.$$

Hence (2.6) follows at once from (2.5)₄.

In conclusion, the voltage excitation problem can also be written as the eddy current problem with the boundary conditions (2.3) and the additional condition (2.6).

Since σ is vanishing in Ω_I , the electric field \mathbf{E}_I is not present in the Ampère equation (2.2)₂. Therefore one can face the problem by splitting it in two steps: in the first step one considers the problem of finding \mathbf{H} in Ω and \mathbf{E}_C in Ω_C , satisfying the Faraday equation (2.2)₁ only in Ω_C , the Ampère equation (2.2)₂ in Ω , with right hand side $\sigma\mathbf{E}_C + \mathbf{J}_C$ in Ω_C and right hand side \mathbf{J}_I in Ω_I , and the magnetic Gauss equation (2.2)₃ in Ω . In the second step the electric field in the non-conducting domain Ω_I has to be obtained by solving, for each $t \in [0, T]$, the curl–div system

$$\begin{aligned} \operatorname{curl} \mathbf{E}_I(t) &= -\mu \frac{\partial \mathbf{H}_I}{\partial t}(t) && \text{on } \Omega_I \\ \operatorname{div}(\varepsilon_I \mathbf{E}_I(t)) &= 0 && \text{on } \Omega_I \\ \varepsilon_I \mathbf{E}_I(t) \cdot \mathbf{n}_I &= 0 && \text{on } \Gamma_I \\ \mathbf{E}_I(t) \times \mathbf{n}_I &= -\mathbf{E}_C(t) \times \mathbf{n}_C && \text{on } \Gamma. \end{aligned} \tag{2.7}$$

We refer to [3, Chap. 8] for the results concerning the solvability of this problem. Note that the first equation in (2.7) is nothing else than the Faraday equation in Ω_I , and that the matching condition (2.7)₄ assures that the electric field defined by \mathbf{E}_C in Ω_C and \mathbf{E}_I in Ω_I has a well-defined curl, thus it satisfies the Faraday equation in the whole Ω .

In conclusion, if we are able to find, as indicated above, the magnetic field \mathbf{H} in $\Omega \times (0, T)$ and the electric field \mathbf{E}_C in $\Omega_C \times (0, T)$, for any fixed time t the determination of \mathbf{E}_I can be done as a successive step (or even avoided, if the knowledge of the physical quantity \mathbf{E}_I is not important in the problem at hand).

In view of the Ampère equation (2.2)₂ in Ω_C , we can write

$$\mathbf{E}_C = \sigma^{-1}(\operatorname{curl} \mathbf{H}_C - \mathbf{J}),$$

hence it is also possible to formulate the first step of the solving procedure described above in terms of the magnetic field only. This will be apparent in the next section.

3 Weak formulation

We start reminding the definition of the (real) Hilbert spaces $H(\text{curl}; \Omega)$, $H(\text{div}; \Omega)$. They are defined as follows:

$$H(\text{curl}; \Omega) := \{\mathbf{w} : \Omega \mapsto \mathbb{R}^3 \mid \mathbf{w} \in L^2(\Omega)^3, \text{curl } \mathbf{w} \in L^2(\Omega)^3\},$$

with the norm

$$\|\mathbf{w}\|_{\text{curl}, \Omega}^2 := \|\mathbf{w}\|_{L^2(\Omega)^3}^2 + \|\text{curl } \mathbf{w}\|_{L^2(\Omega)^3}^2,$$

and

$$H(\text{div}; \Omega) := \{\mathbf{w} : \Omega \mapsto \mathbb{R}^3 \mid \mathbf{w} \in L^2(\Omega)^3, \text{div } \mathbf{w} \in L^2(\Omega)\},$$

with the norm

$$\|\mathbf{w}\|_{\text{div}, \Omega}^2 := \|\mathbf{w}\|_{L^2(\Omega)^3}^2 + \|\text{div } \mathbf{w}\|_{L^2(\Omega)}^2.$$

Here and in the sequel, the differential operators are defined in the distributional sense.

We also need to recall some properties of the vector functions belonging either to $H(\text{curl}; \Omega)$ or to $H(\text{div}; \Omega)$ (see, e.g., [19], p. 107). For all $\mathbf{w} \in H(\text{curl}; \Omega)$, we know that the tangential trace is continuous on interfaces, in particular

$$\mathbf{w}_C \times \mathbf{n}_C = -\mathbf{w}_I \times \mathbf{n}_I \quad \text{on } \Gamma, \quad \mathbf{w} \in H(\text{curl}; \Omega), \quad (3.8)$$

the minus sign being due to the fact that on the interface Γ we have $\mathbf{n}_C = -\mathbf{n}_I$. For all $\mathbf{w} \in H(\text{div}; \Omega)$, we know that the normal trace is continuous on interfaces, in particular

$$\mathbf{w}_C \cdot \mathbf{n}_C = -\mathbf{w}_I \cdot \mathbf{n}_I \quad \text{on } \Gamma, \quad \mathbf{w} \in H(\text{div}; \Omega). \quad (3.9)$$

Moreover, we also have that all $\mathbf{w} \in H(\text{curl}; \Omega)$ satisfy (in a suitable weak sense)

$$\text{div}_\tau(\mathbf{w} \times \mathbf{n}) = \text{curl } \mathbf{w} \cdot \mathbf{n} \quad \text{on } \Sigma, \quad (3.10)$$

where Σ is any Lipschitz surface contained on $\overline{\Omega}$ (see, e.g., [19], p. 59; [3], p. 313).

To set up a weak formulation of the eddy current problem, we introduce the spaces

$$\begin{aligned} \mathbf{W} &= \{\mathbf{w} \in H(\text{curl}; \Omega) \mid \text{curl } \mathbf{w}_I = \mathbf{0} \text{ in } \Omega_I\} \\ \mathbf{X} &= \{\mathbf{w} \in L^2(\Omega)^3 \mid \text{curl } \mathbf{w}_I = \mathbf{0} \text{ in } \Omega_I\}. \end{aligned} \quad (3.11)$$

The former is endowed with the scalar product and norm induced by $H(\text{curl}; \Omega)$; for reasons that will be clear later, the latter is endowed with the scalar product

$$(\mathbf{w}, \mathbf{q})_{\mathbf{X}} := \int_{\Omega} \mu \mathbf{w} \cdot \mathbf{q} \quad (3.12)$$

and the associated norm $\|\cdot\|_{\mathbf{X}}$, which are equivalent to the standard scalar product and norm in $L^2(\Omega)^3$.

It is straightforward to check that they are closed subspaces of $H(\text{curl}; \Omega)$ and $L^2(\Omega)^3$, respectively. Since $H(\text{curl}; \Omega)$ and $L^2(\Omega)^3$ are separable Hilbert spaces, \mathbf{W} and \mathbf{X} are separable Hilbert spaces, too.

Before starting to derive the weak formulation, let us warn the reader that for convenience duality pairings are simply expressed by integrals. For instance, $\int_{\partial\Omega} \mathbf{n} \times \mathbf{E}(t) \cdot \mathbf{w}$ means $\langle \mathbf{n} \times \mathbf{E}(t), \mathbf{n} \times \mathbf{w} \times \mathbf{n} \rangle$, i.e., the duality pairing between the space of tangential traces $\mathbf{n} \times \mathbf{E}$ and the tangential components $\mathbf{n} \times \mathbf{w} \times \mathbf{n}$ for $\mathbf{E} \in H(\text{curl}; \Omega)$ and $\mathbf{w} \in H(\text{curl}; \Omega)$.

Similarly, $\int_{\Gamma} \text{curl } \mathbf{w}_C \cdot \mathbf{n}_C$ means $\langle \text{curl } \mathbf{w}_C \cdot \mathbf{n}_C, 1 \rangle$ with the duality pairing between the Sobolev spaces $H^{-1/2}(\Gamma)$ and $H^{1/2}(\Gamma)$.

Multiplying the Faraday equation (2.2)₁ by $\mathbf{w} \in \mathbf{W}$, integrating in Ω , and integrating by parts we find for $t \in (0, T)$:

$$\begin{aligned} 0 &= \int_{\Omega} \mu \frac{\partial \mathbf{H}}{\partial t}(t) \cdot \mathbf{w} + \int_{\Omega} \text{curl } \mathbf{E}(t) \cdot \mathbf{w} \\ &= \int_{\Omega} \mu \frac{\partial \mathbf{H}}{\partial t}(t) \cdot \mathbf{w} + \int_{\Omega_C} \mathbf{E}_C(t) \cdot \text{curl } \mathbf{w}_C + \int_{\partial\Omega} (\mathbf{n} \times \mathbf{E}(t)) \cdot \mathbf{w}. \end{aligned} \quad (3.13)$$

Note now that the vector field $\text{curl } \mathbf{w}$ is clearly divergence free in Ω , because $\text{div } \text{curl} = 0$. Therefore, by (3.9) we have that $\text{curl } \mathbf{w}_C \cdot \mathbf{n}_C = -\text{curl } \mathbf{w}_I \cdot \mathbf{n}_I$ on Γ . Looking back at the definition of the space \mathbf{W} , we also know that $\text{curl } \mathbf{w}_I = \mathbf{0}$ in Ω_I , thus we conclude that $\text{curl } \mathbf{w}_C \cdot \mathbf{n}_C = 0$ on Γ . Therefore, the divergence theorem implies

$$0 = \int_{\Omega_C} \text{div } \text{curl } \mathbf{w}_C = \int_{\Gamma \cup \Gamma_J \cup \Gamma_E} \text{curl } \mathbf{w}_C \cdot \mathbf{n}_C = \int_{\Gamma_J \cup \Gamma_E} \text{curl } \mathbf{w}_C \cdot \mathbf{n}_C, \quad (3.14)$$

and hence

$$\int_{\Gamma_E} \text{curl } \mathbf{w}_C \cdot \mathbf{n}_C = - \int_{\Gamma_J} \text{curl } \mathbf{w}_C \cdot \mathbf{n}_C. \quad (3.15)$$

We have now to remind some results. First, from (2.5) we know that $\mathbf{E}(t) \times \mathbf{n} = -\text{grad } v(t) \times \mathbf{n}$ on $\partial\Omega$, and that the potential $v(t)$ has the properties that $v|_{\Gamma_J}(t)$ and $v|_{\Gamma_E}(t)$ do not depend on \mathbf{x} and

$$v|_{\Gamma_J}(t) - v|_{\Gamma_E}(t) = (V_J - V_E)(t).$$

Second, since $\mathbf{w} \in \mathbf{W}$ we know that $\text{curl } \mathbf{w}_I = \mathbf{0}$ in Ω_I and thus $\text{curl } \mathbf{w}_I \cdot \mathbf{n} = 0$ on Γ_I . Third, using an integration by parts formula on the boundary we have

$$\int_{\partial\Omega} (\mathbf{w} \times \mathbf{n}) \cdot \text{grad}_\tau \phi = - \int_{\partial\Omega} \text{div}_\tau (\mathbf{w} \times \mathbf{n}) \phi.$$

Hence the boundary term in (3.13) can be rewritten as

$$\begin{aligned} \int_{\partial\Omega} (\mathbf{n} \times \mathbf{E}(t)) \cdot \mathbf{w} &= - \int_{\partial\Omega} (\mathbf{n} \times \text{grad } v(t)) \cdot \mathbf{w} \\ &= - \int_{\partial\Omega} (\mathbf{w} \times \mathbf{n}) \cdot \text{grad}_\tau v(t) \\ &= \int_{\partial\Omega} \text{div}_\tau (\mathbf{w} \times \mathbf{n}) v(t) = \int_{\partial\Omega} (\text{curl } \mathbf{w} \cdot \mathbf{n}) v(t) \\ &= \int_{\Gamma_J \cup \Gamma_E} (\text{curl } \mathbf{w}_C \cdot \mathbf{n}_C) v(t) \\ &= v|_{\Gamma_J}(t) \int_{\Gamma_J} \text{curl } \mathbf{w}_C \cdot \mathbf{n}_C + v|_{\Gamma_E}(t) \int_{\Gamma_E} \text{curl } \mathbf{w}_C \cdot \mathbf{n}_C \\ &= (V_J(t) - V_E(t)) \int_{\Gamma_J} \text{curl } \mathbf{w}_C \cdot \mathbf{n}_C, \end{aligned} \tag{3.16}$$

having used (3.10) in the fourth equality and (3.15) in the last one.

Using the Ampère equation (2.2)₂ in Ω_C we obtain

$$\mathbf{E}_C(t) = \sigma^{-1}(\text{curl } \mathbf{H}_C(t) - \mathbf{J}_C(t)),$$

therefore (3.13) becomes

$$\begin{aligned} \frac{d}{dt} \int_{\Omega} \mu \mathbf{H}(t) \cdot \mathbf{w} + \int_{\Omega_C} \sigma^{-1} \text{curl } \mathbf{H}_C(t) \cdot \text{curl } \mathbf{w}_C \\ = \int_{\Omega_C} \sigma^{-1} \mathbf{J}_C(t) \cdot \text{curl } \mathbf{w}_C - (V_J - V_E)(t) \int_{\Gamma_J} \text{curl } \mathbf{w}_C \cdot \mathbf{n}_C. \end{aligned} \tag{3.17}$$

On the other hand we also have the Ampère equation (2.2)₂ in Ω_I , namely,

$$\text{curl } \mathbf{H}_I = \mathbf{J}_I \text{ in } \Omega_I.$$

For the sake of simplicity, from now on we assume that $\mathbf{J}_I = \mathbf{0}$ in Ω_I (the general case can be treated by following the arguments in [3, Chap. 8]). By this assumption we have that the Ampère equation in Ω_I becomes $\text{curl } \mathbf{H}_I = \mathbf{0}$.

Problem 1. *The weak formulation of the eddy current problem reads as follows: given the data $\mathbf{J}_C \in L^2(0, T; L^2(\Omega_C)^3)$, $V_J \in L^2(0, T)$, $V_E \in L^2(0, T)$ and $\mathbf{H}_0 \in \mathbf{X}$ with $\text{div}(\mu \mathbf{H}_0) = 0$ in Ω and $\mu \mathbf{H}_0 \cdot \mathbf{n} = 0$ on $\partial\Omega$, find $\mathbf{H} \in L^2(0, T; \mathbf{W}) \cap C^0([0, T]; \mathbf{X})$ such that*

$$\begin{aligned} \frac{d}{dt} \int_{\Omega} \mu \mathbf{H}(t) \cdot \mathbf{w} + \int_{\Omega_C} \sigma^{-1} \text{curl } \mathbf{H}_C(t) \cdot \text{curl } \mathbf{w}_C \\ = \int_{\Omega_C} \sigma^{-1} \mathbf{J}_C(t) \cdot \text{curl } \mathbf{w}_C - (V_J - V_E)(t) \int_{\Gamma_J} \text{curl } \mathbf{w}_C \cdot \mathbf{n}_C, \end{aligned} \quad (3.18)$$

for all $\mathbf{w} \in \mathbf{W}$ and a.a. $t \in (0, T)$, and

$$\mathbf{H}|_{t=0} = \mathbf{H}_0 \text{ in } \Omega. \quad (3.19)$$

Note that, indeed, it would be enough to assume that the voltage drop $V_J - V_E$ belongs to $L^2(0, T)$.

Proving well-posedness of this problem is an easy task.

Theorem 3.1. *For all $\mathbf{J}_C \in L^2(0, T; L^2(\Omega_C)^3)$, $V_J \in L^2(0, T)$, $V_E \in L^2(0, T)$ and $\mathbf{H}_0 \in \mathbf{X}$ with $\text{div}(\mu \mathbf{H}_0) = 0$ in Ω and $\mu \mathbf{H}_0 \cdot \mathbf{n} = 0$ on $\partial\Omega$, Problem 1 has a unique solution $\mathbf{H} \in L^2(0, T; \mathbf{W}) \cap C^0([0, T]; \mathbf{X})$.*

Moreover, there is a constant $c_w > 0$ not depending on \mathbf{J}_C , V_J , V_E , and \mathbf{H}_0 such that

$$\begin{aligned} \|\mathbf{H}\|_{L^2(0, T; \mathbf{W})} + \|\mathbf{H}\|_{C^0([0, T]; \mathbf{X})} \\ \leq c_w \left(\|\mathbf{J}_C\|_{L^2(0, T; L^2(\Omega_C)^3)} + \|V_J - V_E\|_{L^2(0, T)} + \|\mathbf{H}_0\|_{L^2(\Omega_C)^3} \right). \end{aligned} \quad (3.20)$$

Proof. The existence and uniqueness theory for this problem can be easily brought back to classical results, for instance the Lions theorem (see, e.g., [8], pp. 512–513). The couple of separable Hilbert spaces is given by \mathbf{W} and \mathbf{X} , with $\mathbf{W} \subset \mathbf{X}$; let us remind that \mathbf{X} is endowed with the scalar product (3.12).

By [5, Lemma 3.2] we know that \mathbf{W} is dense in \mathbf{X} . Finally, the bilinear form

$$a(\mathbf{H}, \mathbf{w}) = \int_{\Omega_C} \sigma^{-1} \text{curl } \mathbf{H}_C \cdot \text{curl } \mathbf{w}_C \quad (3.21)$$

satisfies

$$a(\mathbf{w}, \mathbf{w}) + \beta \|\mathbf{w}\|_{\mathbf{X}}^2 \geq \alpha \|\mathbf{w}\|_W^2 \quad (3.22)$$

for suitable constants $\beta > 0$ and $\alpha > 0$ (say, $\alpha = \sigma_{\max}^{-1}$, $\beta = \sigma_{\max}^{-1} \mu_{\min}^{-1}$, where σ_{\max} is an upper bound for the maximum eigenvalue of $\sigma(\mathbf{x})$ in Ω_C and μ_{\min} is a lower bound for the minimum eigenvalue of $\mu(\mathbf{x})$ in Ω), and thus all the hypotheses in [8], Theor. 1, pp. 512–513, are fulfilled. \square

4 Strong formulation

Let us furnish the strong interpretation of the variational problem (3.18), as it is interesting in itself, and moreover can be the starting point for numerical approximation not based on variational methods.

We start by defining the space of harmonic fields

$$\mathcal{H}_I^\mu = \{\mathbf{v} : \Omega_I \mapsto \mathbb{R}^3 \mid \text{curl } \mathbf{v} = \mathbf{0} \text{ in } \Omega_I, \text{div}(\mu \mathbf{v}) = 0 \text{ in } \Omega_I, \mu \mathbf{v} \cdot \mathbf{n} = 0 \text{ on } \partial\Omega_I\}. \quad (4.23)$$

Here we have used the weight μ for orthogonality reasons (see (4.26) and (4.27)), as the scalar product in \mathbf{X} is given by (3.12).

This space is trivial if and only if the domain Ω_I is simply-connected. Its dimension coincides with the dimension of the first homology group of $\overline{\Omega}_I$, namely, the first Betti number of Ω_I . From a geometrical point of view, the first Betti number is the number of “handles” of the domain.

In the geometrical situation we are considering the space \mathcal{H}_I^μ has dimension 1. We denote by $\boldsymbol{\rho}$ the basis function satisfying the normalization condition

$$\oint_{\partial^+\Gamma_J} \boldsymbol{\rho} \cdot \boldsymbol{\tau}_J^+ = 1. \quad (4.24)$$

By the notation $\partial^+\Gamma_J$ we mean that the associated tangent vector $\boldsymbol{\tau}_J^+$ is given by

$$\boldsymbol{\tau}_J^+ = \kappa_J \mathbf{n}_{C|\Gamma_J} \times \mathbf{n}_{C|\Gamma},$$

where $\kappa_J = |\mathbf{n}_{C|\Gamma_J} \times \mathbf{n}_{C|\Gamma}|^{-1}$ is just a normalizing factor. Note that, by the assumption on the geometry 2.1, we know that the intersection of Γ_C and Γ is transversal, thus $\mathbf{n}_{C|\Gamma_J}$ and $\mathbf{n}_{C|\Gamma}$ are not parallel.

On the other electric port Γ_E we define

$$\boldsymbol{\tau}_E^+ = -\kappa_E \mathbf{n}_{C|\Gamma_E} \times \mathbf{n}_{C|\Gamma},$$

with $\kappa_E = |\mathbf{n}_{C|\Gamma_E} \times \mathbf{n}_{C|\Gamma}|^{-1}$; in this way the two closed cycles $\partial^+\Gamma_J$ and $\partial^+\Gamma_E$ are homologically equivalent, and, due to the fact that $\boldsymbol{\rho}$ is curl free, we have

$$\oint_{\partial^+\Gamma_E} \boldsymbol{\rho} \cdot \boldsymbol{\tau}_E^+ = 1 \quad (4.25)$$

as well.

Since the domain Ω_I is not simply-connected, though the magnetic field \mathbf{H}_I is curl free in Ω_I it is not possible to represent it as a gradient. However, it is the sum of a gradient plus a vector field belonging to \mathcal{H}_I^μ .

More precisely, for each $t \in [0, T]$ we can write

$$\mathbf{H}_I(t) = \text{grad } \psi_I(t) + I^0(t)\boldsymbol{\rho}, \quad (4.26)$$

where $\psi_I(t) \in H^1(\Omega_I)/\mathbb{R}$ and $I^0(t) \in \mathbb{R}$. It is also easily verified that the two terms in this decomposition are orthogonal in \mathbf{X} , as by integration by parts we obtain at once

$$\int_{\Omega_I} \mu \text{grad } \eta_I \cdot \boldsymbol{\rho} = 0 \quad \forall \eta_I \in H^1(\Omega_I) \quad (4.27)$$

since $\boldsymbol{\rho} \in \mathcal{H}_I^\mu$.

Let us explain the physical interpretation of the function $t \mapsto I^0(t)$. Since $\partial^+\Gamma_J$ is a closed curve contained in $\overline{\Omega_I}$, we clearly have

$$\begin{aligned} \oint_{\partial^+\Gamma_J} \mathbf{H}_I(t) \cdot \boldsymbol{\tau}_J^+ &= \oint_{\partial^+\Gamma_J} (\text{grad } \psi_I(t) + I^0(t)\boldsymbol{\rho}) \cdot \boldsymbol{\tau}_J^+ \\ &= I^0(t) \oint_{\partial^+\Gamma_J} \boldsymbol{\rho} \cdot \boldsymbol{\tau}_J^+ = I^0(t). \end{aligned}$$

Due to the matching condition $\mathbf{H}_C(t) \times \mathbf{n}_C = \mathbf{H}_I(t) \times \mathbf{n}_C$ on Γ , by a direct manipulation we find

$$\begin{aligned} \oint_{\partial^+\Gamma_J} \mathbf{H}_I(t) \cdot \boldsymbol{\tau}_J^+ &= \oint_{\partial^+\Gamma_J} \mathbf{H}_I(t) \cdot \kappa_J (\mathbf{n}_{C|\Gamma_J} \times \mathbf{n}_{C|\Gamma}) \\ &= - \oint_{\partial^+\Gamma_J} \kappa_J (\mathbf{H}_I(t) \times \mathbf{n}_{C|\Gamma}) \cdot \mathbf{n}_{C|\Gamma_J} \\ &= - \oint_{\partial^+\Gamma_J} \kappa_J (\mathbf{H}_C(t) \times \mathbf{n}_{C|\Gamma}) \cdot \mathbf{n}_{C|\Gamma_J} \\ &= \oint_{\partial^+\Gamma_J} \kappa_J \mathbf{H}_C(t) \cdot (\mathbf{n}_{C|\Gamma_J} \times \mathbf{n}_{C|\Gamma}) = \oint_{\partial^+\Gamma_J} \mathbf{H}_C(t) \cdot \boldsymbol{\tau}_J^+. \end{aligned} \quad (4.28)$$

The closed curve $\partial^+\Gamma_J$ is not the boundary of a surface contained in $\overline{\Omega_I}$, but it is the boundary of Γ_J , and the surface Γ_J is a part of the boundary of Ω_C . Therefore, by the Stokes theorem we obtain

$$I^0(t) = \oint_{\partial^+\Gamma_J} \mathbf{H}_C(t) \cdot \boldsymbol{\tau}_J^+ = \int_{\Gamma_J} \operatorname{curl} \mathbf{H}_C(t) \cdot \mathbf{n}_C = \int_{\Gamma_J} (\sigma \mathbf{E}_C(t) + \mathbf{J}_C(t)) \cdot \mathbf{n}_C.$$

This shows that $I^0(t)$ is the total current intensity passing at time t through Γ_J in the direction of \mathbf{n}_C .

We are now in a position to state the following formal result:

Theorem 4.1. *In terms of the magnetic field \mathbf{H} only, the strong form of problem (3.18) is the following:*

$$\begin{aligned} \mu \frac{\partial \mathbf{H}_C}{\partial t} + \operatorname{curl}(\sigma^{-1} \operatorname{curl} \mathbf{H}_C) &= \operatorname{curl}(\sigma^{-1} \mathbf{J}_C) && \text{in } \Omega_C \times (0, T) \\ \operatorname{div}(\mu \mathbf{H}) &= 0 && \text{in } \Omega \times (0, T) \\ \operatorname{curl} \mathbf{H}_I &= \mathbf{0} && \text{in } \Omega_I \times (0, T) \\ \mathbf{H}_C \times \mathbf{n}_C + \mathbf{H}_I \times \mathbf{n}_I &= \mathbf{0} && \text{on } \Gamma \times (0, T) \\ (\sigma^{-1} \operatorname{curl} \mathbf{H}_C) \times \mathbf{n}_C &= (\sigma^{-1} \mathbf{J}_C) \times \mathbf{n}_C && \text{on } (\Gamma_J \cup \Gamma_E) \times (0, T) \\ \mu \mathbf{H} \cdot \mathbf{n} &= 0 && \text{on } \partial\Omega \times (0, T) \\ \mathbf{H}|_{t=0} &= \mathbf{H}_0 && \text{in } \Omega, \end{aligned} \tag{4.29}$$

along with the voltage condition

$$\begin{aligned} \left(\int_{\Omega_I} \mu \boldsymbol{\rho} \cdot \boldsymbol{\rho} \right) \frac{dI^0}{dt} + \int_{\Gamma} \sigma^{-1} \operatorname{curl} \mathbf{H}_C \cdot (\boldsymbol{\rho} \times \mathbf{n}_I) \\ = -(V_J - V_E) + \int_{\Gamma} \sigma^{-1} \mathbf{J}_C \cdot (\boldsymbol{\rho} \times \mathbf{n}_I) \quad \text{in } (0, T), \end{aligned} \tag{4.30}$$

where $I^0(t) := \oint_{\partial^+\Gamma_J} \mathbf{H}_I(t) \cdot \boldsymbol{\tau}_J^+$ (and, clearly, $I^0(0) := \oint_{\partial^+\Gamma_J} \mathbf{H}_{0,I} \cdot \boldsymbol{\tau}_J^+$).

Proof. The conditions $\operatorname{curl} \mathbf{H}_I = \mathbf{0}$ in Ω_I and $\mathbf{H}_C \times \mathbf{n}_C = -\mathbf{H}_I \times \mathbf{n}_I$ on Γ are satisfied as $\mathbf{H} \in \mathbf{W}$, while the condition $\mathbf{H}|_{t=0} = \mathbf{H}_0$ in Ω is explicitly stated in the weak formulation (see (3.19)).

The Faraday equation (4.29)₁ follows straightforwardly taking in the weak formulation (3.18) a test function $\mathbf{w} \in C^\infty(\Omega)^3$ with $\operatorname{supp} \mathbf{w} \subset \Omega_C$ and integrating by parts.

We can repeat the same computation with a test function $\mathbf{w} \in H(\operatorname{curl}; \Omega)$ with $\mathbf{w}_I = \mathbf{0}$ in Ω_I (hence $\mathbf{w}_C \times \mathbf{n}_C = \mathbf{0}$ on Γ by (3.8)) and

$\mathbf{w}_C \times \mathbf{n}_C = \mathbf{0}$ on Γ_E . Recalling that $\partial\Omega_C = \Gamma \cup \Gamma_J \cup \Gamma_E$ it follows that

$$\begin{aligned} & \int_{\Omega_C} \left(\mu \frac{\partial \mathbf{H}_C}{\partial t} + \text{curl}[\sigma^{-1}(\text{curl} \mathbf{H}_C - \mathbf{J}_C)] \right) \cdot \mathbf{w}_C \\ & + \int_{\Gamma_J} \sigma^{-1}(\text{curl} \mathbf{H}_C - \mathbf{J}_C) \cdot (\mathbf{n}_C \times \mathbf{w}_C) \\ & = -(V_J - V_E) \int_{\Gamma_J} \text{curl} \mathbf{w}_C \cdot \mathbf{n}_C. \end{aligned}$$

Using the Faraday equation (4.29)₁ just obtained in Ω_C we find

$$\int_{\Gamma_J} ([\sigma^{-1}(\text{curl} \mathbf{H}_C - \mathbf{J}_C)] \times \mathbf{n}_C) \cdot \mathbf{w}_C = -(V_J - V_E) \int_{\Gamma_J} \text{curl} \mathbf{w}_C \cdot \mathbf{n}_C.$$

In (3.15) we have proved that for $\mathbf{w} \in \mathbf{W}$ it holds $\int_{\Gamma_J} \text{curl} \mathbf{w}_C \cdot \mathbf{n}_C = -\int_{\Gamma_E} \text{curl} \mathbf{w}_C \cdot \mathbf{n}_C$. Since by (3.10) we have $\text{curl} \mathbf{w}_C \cdot \mathbf{n}_C = \text{div}_\tau(\mathbf{w}_C \times \mathbf{n}_C) = 0$ on Γ_E , in the present situation we have $\int_{\Gamma_J} \text{curl} \mathbf{w}_C \cdot \mathbf{n}_C = 0$, hence

$$\int_{\Gamma_J} ([\sigma^{-1}(\text{curl} \mathbf{H}_C - \mathbf{J}_C)] \times \mathbf{n}_C) \cdot \mathbf{w}_C = 0.$$

Since \mathbf{w} is arbitrary on Γ_J , we have therefore obtained

$$[\sigma^{-1}(\text{curl} \mathbf{H}_C - \mathbf{J}_C)] \times \mathbf{n}_C = \mathbf{0} \quad \text{on } \Gamma_J.$$

Converting the role of Γ_J and Γ_E , we obtain the same result on Γ_E , proving that (4.29)₅ is satisfied.

Now we choose $\mathbf{w} = \text{grad } \eta$ with $\eta \in C_0^\infty(\Omega)$. We find

$$\frac{d}{dt} \int_{\Omega} \mu \mathbf{H} \cdot \text{grad } \eta = 0,$$

hence $\int_{\Omega} \mu \mathbf{H} \cdot \text{grad } \eta$ is independent of t . Integrating by parts, we see that the same is true for $\int_{\Omega} \text{div}(\mu \mathbf{H}) \eta$. Using that the initial datum \mathbf{H}_0 satisfies $\text{div}(\mu \mathbf{H}_0) = 0$ in Ω , we obtain

$$\int_{\Omega} \text{div}(\mu \mathbf{H}(t)) \eta = \int_{\Omega} \text{div}(\mu \mathbf{H}_0) \eta = 0.$$

Due to the fact that η is arbitray, this gives equation (4.29)₂.

The choice $\mathbf{w} = \text{grad } \eta$ with $\eta \in H^1(\Omega)$ furnishes, integrating by parts,

$$0 = \frac{d}{dt} \int_{\Omega} \mu \mathbf{H} \cdot \text{grad } \eta = -\frac{d}{dt} \int_{\Omega} \text{div}(\mu \mathbf{H}) \eta + \frac{d}{dt} \int_{\partial\Omega} \mu \mathbf{H} \cdot \mathbf{n} \eta = \frac{d}{dt} \int_{\partial\Omega} \mu \mathbf{H} \cdot \mathbf{n} \eta.$$

Therefore, $\int_{\partial\Omega} \mu \mathbf{H} \cdot \mathbf{n} \eta$ is independent of t . Using that the initial datum satisfies $\mu \mathbf{H}_0 \cdot \mathbf{n} = 0$ on $\partial\Omega$, it follows

$$\int_{\partial\Omega} \mu \mathbf{H}(t) \cdot \mathbf{n} \eta = \int_{\partial\Omega} \mu \mathbf{H}_0 \cdot \mathbf{n} \eta = 0,$$

namely, since η is arbitrary on $\partial\Omega$, equation (4.29)₆.

Finally, take in (3.18) a test function $\mathbf{w} \in \mathbf{W}$ with $\mathbf{w}|_{\Omega_I} = \boldsymbol{\rho}$. Integrating by parts we first find

$$\begin{aligned} & \int_{\Omega_C} \sigma^{-1}(\operatorname{curl} \mathbf{H}_C - \mathbf{J}_C) \cdot \operatorname{curl} \mathbf{w}_C \\ &= \int_{\Omega_C} \operatorname{curl}[\sigma^{-1}(\operatorname{curl} \mathbf{H}_C - \mathbf{J}_C)] \cdot \mathbf{w}_C \\ & \quad + \int_{\Gamma} [\sigma^{-1}(\operatorname{curl} \mathbf{H}_C - \mathbf{J}_C)] \cdot (\mathbf{n}_C \times \mathbf{w}_C). \end{aligned}$$

The Faraday equation (4.29)₁ reads

$$\operatorname{curl}[\sigma^{-1}(\operatorname{curl} \mathbf{H}_C - \mathbf{J}_C)] = -\mu \frac{\partial \mathbf{H}_C}{\partial t};$$

using it along with relation (3.8) that gives $\mathbf{n}_C \times \mathbf{w}_C = \mathbf{w}_I \times \mathbf{n}_I = \boldsymbol{\rho} \times \mathbf{n}_I$, we are left with

$$\begin{aligned} & \frac{d}{dt} \int_{\Omega_I} \mu \mathbf{H}_I \cdot \boldsymbol{\rho} + \int_{\Gamma} [\sigma^{-1}(\operatorname{curl} \mathbf{H}_C - \mathbf{J}_C)] \cdot (\boldsymbol{\rho} \times \mathbf{n}_I) \\ &= -(V_J - V_E) \int_{\Gamma_J} \operatorname{curl} \mathbf{w}_C \cdot \mathbf{n}_C. \end{aligned} \quad (4.31)$$

By the Stokes theorem, it follows $\int_{\Gamma_J} \operatorname{curl} \mathbf{w}_C \cdot \mathbf{n}_C = \oint_{\partial^+ \Gamma_J} \mathbf{w}_C \cdot \boldsymbol{\tau}_J^+$. Moreover, as in (4.28), we have $\oint_{\partial^+ \Gamma_J} \mathbf{w}_C \cdot \boldsymbol{\tau}_J^+ = \oint_{\partial^+ \Gamma_J} \mathbf{w}_I \cdot \boldsymbol{\tau}_J^+$; since the test function \mathbf{w} we are using satisfies $\mathbf{w}|_{\Omega_I} = \mathbf{w}_I = \boldsymbol{\rho}$, we rewrite this relation as $\oint_{\partial^+ \Gamma_J} \mathbf{w}_C \cdot \boldsymbol{\tau}_J^+ = \oint_{\partial^+ \Gamma_J} \boldsymbol{\rho} \cdot \boldsymbol{\tau}_J^+$. Because by (4.24) it holds $\oint_{\partial^+ \Gamma_J} \boldsymbol{\rho} \cdot \boldsymbol{\tau}_J^+ = 1$, we have at last

$$\int_{\Gamma_J} \operatorname{curl} \mathbf{w}_C \cdot \mathbf{n}_C = 1. \quad (4.32)$$

Finally, since from (4.26) and (4.27) we can write $\mathbf{H}_I(t) = \operatorname{grad} \psi_I(t) + \Gamma^0(t) \boldsymbol{\rho}$ with $\int_{\Omega_I} \mu \operatorname{grad} \psi_I \cdot \boldsymbol{\rho} = 0$, we conclude

$$\frac{d}{dt} \int_{\Omega_I} \mu \mathbf{H}_I \cdot \boldsymbol{\rho} = \frac{d}{dt} \int_{\Omega_I} \mu (\operatorname{grad} \psi_I + \Gamma^0 \boldsymbol{\rho}) \cdot \boldsymbol{\rho} = \frac{d\Gamma^0}{dt} \left(\int_{\Omega_I} \mu \boldsymbol{\rho} \cdot \boldsymbol{\rho} \right),$$

and equation (4.30) follows readily from this last relation, (4.31) and (4.32). \square

Remark 2. Setting $\mathbf{E}_C = \sigma^{-1}(\text{curl } \mathbf{H}_C - \mathbf{J}_C)$ in Ω_C , it is clearly verified that with this definition the Ampère equation in Ω_C is satisfied; moreover, (4.29)₁ can be read as the Faraday equation in Ω_C .

The proof that the solution to the variational problem (3.18) satisfies the boundary conditions (2.5)₂–(2.5)₅ needs some additional effort. First of all, to determine the electric field \mathbf{E} globally in Ω , one has to solve problem (2.7). Then we can conclude as follows:

Theorem 4.2. Let \mathbf{H} be the weak solution of problem (3.18). Then problem (2.7) has a unique solution \mathbf{E}_I in Ω_I (in particular, (2.5)₅ is satisfied). Moreover, the electric field given by $\mathbf{E}_C = \sigma^{-1}(\text{curl } \mathbf{H}_C - \mathbf{J}_C)$ in Ω_C and by the solution \mathbf{E}_I to problem (2.7) in Ω_I satisfies (2.5)₂–(2.5)₄.

Proof. For the solvability of problem (2.7) refer to [3, Theor. 8.6] (the only difference being that there the right hand side comes from the time-harmonic expression of the time-derivative).

From the Faraday equation, the boundary condition (4.29)₆ and (3.10) we know that

$$\text{div}_\tau(\mathbf{E} \times \mathbf{n}) = \text{curl } \mathbf{E} \cdot \mathbf{n} = 0 \text{ on } \partial\Omega \times (0, T).$$

Since $\partial\Omega$ is simply connected, for each $t \in (0, T)$ from (2.4) we have that (2.5)₂ is satisfied, i.e.,

$$\mathbf{E} \times \mathbf{n} = -\text{grad } v \times \mathbf{n} \text{ on } \partial\Omega. \quad (4.33)$$

Let us indicate the boundary values of the function v on Γ_J and Γ_E by $v|_{\Gamma_J} = U_J$ and $v|_{\Gamma_E} = U_E$. Since we have defined $\mathbf{E}_C = \sigma^{-1}(\text{curl } \mathbf{H}_C - \mathbf{J}_C)$ in Ω_C , the boundary condition (4.29)₅ states that $\mathbf{E}_C \times \mathbf{n}_C = \mathbf{0}$ on $\Gamma_J \cup \Gamma_E$, namely, by (4.33), $\text{grad } v|_{\Omega_C} \times \mathbf{n}_C = \mathbf{0}$ on $\Gamma_J \cup \Gamma_E$. Both surfaces Γ_J and Γ_E are connected, thus we deduce that U_J and U_E do not depend on the space variable, which is condition (2.5)₃.

As seen before in (4.31) and (4.32), the voltage condition (4.30) can be also written as

$$\frac{d}{dt} \int_{\Omega_I} \mu \mathbf{H}_I \cdot \boldsymbol{\rho} + \int_{\Gamma} \mathbf{E}_C \cdot (\boldsymbol{\rho} \times \mathbf{n}_I) = -(V_J - V_E).$$

By the matching condition (2.7)₄ on Γ , this is equivalent to

$$\begin{aligned} \frac{d}{dt} \int_{\Omega_I} \mu \mathbf{H}_I \cdot \boldsymbol{\rho} + \int_{\Gamma \cup (\partial\Omega \cap \partial\Omega_I)} \mathbf{E}_I \cdot (\boldsymbol{\rho} \times \mathbf{n}_I) \\ - \int_{\partial\Omega \cap \partial\Omega_I} \mathbf{E}_I \cdot (\boldsymbol{\rho} \times \mathbf{n}_I) = -(V_J - V_E). \end{aligned} \quad (4.34)$$

We have $\Gamma \cup (\partial\Omega \cap \partial\Omega_I) = \partial\Omega_I$, hence integration by parts yields

$$\int_{\Gamma \cup (\partial\Omega \cap \partial\Omega_I)} \mathbf{E}_I \cdot (\boldsymbol{\rho} \times \mathbf{n}_I) = \int_{\Omega_I} \operatorname{curl} \mathbf{E}_I \cdot \boldsymbol{\rho},$$

having used that $\operatorname{curl} \boldsymbol{\rho} = \mathbf{0}$ in Ω_I . This relation and Faraday equation (2.7)₁ permit to rewrite (4.34) as

$$- \int_{\partial\Omega \cap \partial\Omega_I} \mathbf{E}_I \cdot (\boldsymbol{\rho} \times \mathbf{n}_I) = -(V_J - V_E). \quad (4.35)$$

By (4.33) we have $\mathbf{E} \times \mathbf{n} = -\operatorname{grad} v \times \mathbf{n}$ on $\partial\Omega$, hence the left hand side of (4.35) is given by

$$\begin{aligned} - \int_{\partial\Omega \cap \partial\Omega_I} \mathbf{E}_I \cdot (\boldsymbol{\rho} \times \mathbf{n}_I) &= \int_{\partial\Omega \cap \partial\Omega_I} \mathbf{E}_I \times \mathbf{n}_I \cdot \boldsymbol{\rho} \\ &= - \int_{\partial\Omega \cap \partial\Omega_I} \operatorname{grad} v \times \mathbf{n}_I \cdot \boldsymbol{\rho} = \int_{\partial\Omega \cap \partial\Omega_I} \operatorname{grad}_\tau v \cdot (\boldsymbol{\rho} \times \mathbf{n}_I). \end{aligned} \quad (4.36)$$

We need now to perform an integration by parts, related to the tangential operators grad_τ and div_τ , on the surface $\partial\Omega \cap \partial\Omega_I$, whose boundary is given by the two curves $\partial\Gamma_J$ and $\partial\Gamma_E$. We set $\boldsymbol{\nu} = \mathbf{n}_I|_{\partial\Omega} \times \boldsymbol{\tau}_J^+$ on $\partial\Gamma_J$ and $\boldsymbol{\nu} = -\mathbf{n}_I|_{\partial\Omega} \times \boldsymbol{\tau}_E^+$ on Γ_E . In this way, $\boldsymbol{\nu}$ is a unit vector, tangential to $\partial\Omega \cap \partial\Omega_I$ and orthogonal to the curves $\partial\Gamma_J$ and $\partial\Gamma_E$; in particular, it points outward $\partial\Omega \cap \partial\Omega_I$, looked as a surface on $\partial\Omega$, on both $\partial\Gamma_J$ and $\partial\Gamma_E$. An integration by parts on the surface $\partial\Omega \cap \partial\Omega_I$ thus gives

$$\begin{aligned} \int_{\partial\Omega \cap \partial\Omega_I} \operatorname{grad}_\tau v \cdot (\boldsymbol{\rho} \times \mathbf{n}_I) \\ = - \int_{\partial\Omega \cap \partial\Omega_I} v \operatorname{div}_\tau (\boldsymbol{\rho} \times \mathbf{n}_I) + \oint_{\partial\Gamma_J \cup \partial\Gamma_E} v \boldsymbol{\nu} \cdot (\boldsymbol{\rho} \times \mathbf{n}_I|_{\partial\Omega}) \\ = -U_J \oint_{\partial\Gamma_J} \boldsymbol{\rho} \cdot (\boldsymbol{\nu} \times \mathbf{n}_I|_{\partial\Omega}) - U_E \oint_{\partial\Gamma_E} \boldsymbol{\rho} \cdot (\boldsymbol{\nu} \times \mathbf{n}_I|_{\partial\Omega}). \end{aligned} \quad (4.37)$$

Here, we took into account that $v|_{\Gamma_J} = U_J$ and $v|_{\Gamma_E} = U_E$ do not depend on \mathbf{x} and that, by (3.10), $\operatorname{div}_\tau (\boldsymbol{\rho} \times \mathbf{n}_I) = \operatorname{curl} \boldsymbol{\rho} \cdot \mathbf{n}_I = 0$ on $\partial\Omega_I$.

By our definitions of $\boldsymbol{\nu}$, it is easy to check that $\boldsymbol{\nu} \times \mathbf{n}_{I|\partial\Omega} = \boldsymbol{\tau}_J^+$ on $\partial\Gamma_J$ and $\boldsymbol{\nu} \times \mathbf{n}_{I|\partial\Omega} = -\boldsymbol{\tau}_J^+$ on $\partial\Gamma_E$. Therefore, $\int_{\partial\Gamma_J} \boldsymbol{\rho} \cdot (\boldsymbol{\nu} \times \mathbf{n}_{I|\partial\Omega}) = \int_{\partial\Gamma_J} \boldsymbol{\rho} \cdot \boldsymbol{\tau}_J^+ = 1$ and $\int_{\partial\Gamma_E} \boldsymbol{\rho} \cdot (\boldsymbol{\nu} \times \mathbf{n}_{I|\partial\Omega}) = -\int_{\partial\Gamma_E} \boldsymbol{\rho} \cdot \boldsymbol{\tau}_J^+ = -1$ follow from (4.24) and (4.25), and from (4.36) and (4.37) we conclude

$$-\int_{\partial\Omega \cap \partial\Omega_I} \mathbf{E}_I \cdot (\boldsymbol{\rho} \times \mathbf{n}_I) = -(U_J - U_E).$$

Hence (4.35) gives $-(U_J - U_E) = -(V_J - V_E)$, and the boundary condition (2.5)₄ follows. \square

4.1 More general geometrical settings

Suppose that the geometrical situation is the one described before, with only one exception: we suppose that $\Gamma_C = \partial\Omega_C \cap \partial\Omega$ is the (disjoint) union of $M + 1$ connected surfaces $\Gamma_E, \Gamma_J^1, \dots, \Gamma_J^M$, $M \geq 2$ (see Figure 2).

Then, for each fixed $t \in [0, T]$, the surface potential $v(t)$ turns out to be equal to a constant $V_k(t)$ on each surface Γ_J^k , $k = 1, \dots, M$, and equal to another constant $V_E(t)$ on Γ_E . Proceeding as in (3.14) and (3.16), the boundary term $\int_{\partial\Omega} (\mathbf{n} \times \mathbf{E}) \cdot \mathbf{w}$ can be written as

$$\begin{aligned} \int_{\partial\Omega} (\mathbf{n} \times \mathbf{E}) \cdot \mathbf{w} &= \sum_{k=1}^M \int_{\Gamma_J^k} (\text{curl } \mathbf{w}_C \cdot \mathbf{n}_C) v_C(t) + \int_{\Gamma_E} (\text{curl } \mathbf{w}_C \cdot \mathbf{n}_C) v_C(t) \\ &= \sum_{k=1}^M V_k(t) \int_{\Gamma_J^k} \text{curl } \mathbf{w}_C \cdot \mathbf{n}_C + V_E(t) \int_{\Gamma_E} \text{curl } \mathbf{w}_C \cdot \mathbf{n}_C \\ &= \sum_{k=1}^M (V_k - V_E)(t) \int_{\Gamma_J^k} \text{curl } \mathbf{w}_C \cdot \mathbf{n}_C, \end{aligned}$$

as $\int_{\Gamma_E} \text{curl } \mathbf{w}_C \cdot \mathbf{n}_C = -\sum_{k=1}^M \int_{\Gamma_J^k} \text{curl } \mathbf{w}_C \cdot \mathbf{n}_C$, because $\text{curl } \mathbf{w}_C$ is divergence free in Ω_C . Therefore, the weak formulation of the problem needs only one change: the right hand side of (3.18) has to be substituted by

$$\int_{\Omega_C} \sigma^{-1} \mathbf{J}_C \cdot \text{curl } \mathbf{w}_C - \sum_{k=1}^M (V_k - V_E)(t) \int_{\Gamma_J^k} \text{curl } \mathbf{w}_C \cdot \mathbf{n}_C.$$

If interested in the strong formulation, a further step can be carried out: in the geometrical situation we are now considering the space of

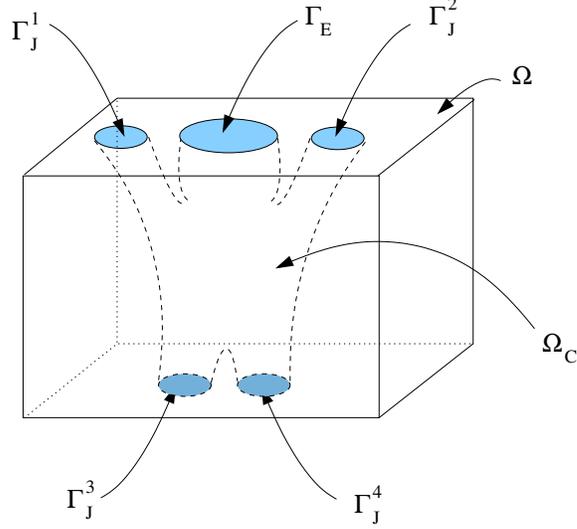


Figure 2: A first alternative geometrical configuration: a connected conductor Ω_C with five electric ports.

harmonic fields \mathcal{H}_I^μ has dimension M , and a basis for it is given by the unique vector fields $\boldsymbol{\rho}_l \in \mathcal{H}_I^\mu$ such that

$$\oint_{\partial+\Gamma_j^k} \boldsymbol{\rho}_l \cdot \boldsymbol{\tau}_{J_k}^+ = \delta_{lk}, \quad l = 1, \dots, M.$$

Taking in the weak formulation a test function $\mathbf{w}_l \in \mathbf{W}$ such $\mathbf{w}_l|_{\Omega_I} = \boldsymbol{\rho}_l$, it is easy to see that equation (4.31) now becomes

$$\begin{aligned} \frac{d}{dt} \int_{\Omega_I} \mu \mathbf{H}_I \cdot \boldsymbol{\rho}_l + \int_{\Gamma} [\sigma^{-1}(\text{curl } \mathbf{H}_C - \mathbf{J}_C)] \cdot (\boldsymbol{\rho}_l \times \mathbf{n}_I) \\ = - \sum_{k=1}^M (V_k - V_E)(t) \int_{\Gamma_j^k} \text{curl } \mathbf{w}_{l,C} \cdot \mathbf{n}_C \end{aligned} \quad (4.38)$$

for $l = 1, \dots, M$. Moreover, proceeding as in the proof of (4.32), by the Stokes theorem one finds

$$\int_{\Gamma_j^k} \text{curl } \mathbf{w}_{l,C} \cdot \mathbf{n}_C = \oint_{\partial+\Gamma_j^k} \mathbf{w}_{l,C} \cdot \boldsymbol{\tau}_J^+.$$

Furthermore, as in (4.28) we have $\oint_{\partial+\Gamma_j^k} \mathbf{w}_{l,C} \cdot \boldsymbol{\tau}_J^+ = \oint_{\partial+\Gamma_j^k} \mathbf{w}_{l,I} \cdot \boldsymbol{\tau}_J^+ = \oint_{\partial+\Gamma_j^k} \boldsymbol{\rho}_l \cdot \boldsymbol{\tau}_J^+$. Hence we have found

$$\int_{\Gamma_j^k} \text{curl } \mathbf{w}_{l,C} \cdot \mathbf{n}_C = \oint_{\partial+\Gamma_j^k} \boldsymbol{\rho}_l \cdot \boldsymbol{\tau}_{J_k}^+ = \delta_{lk}.$$

Finally, writing $\mathbf{H}_I(t) = \text{grad } \psi_I(t) + \sum_{k=1}^M I_k^0(t) \boldsymbol{\rho}_k$ it follows

$$\begin{aligned} \int_{\Omega_I} \mu \mathbf{H}_I(t) \cdot \boldsymbol{\rho}_l &= \int_{\Omega_I} \mu \left(\text{grad } \psi_I(t) + \sum_{k=1}^M I_k^0(t) \boldsymbol{\rho}_k \right) \cdot \boldsymbol{\rho}_l \\ &= \sum_{k=1}^M I_k^0(t) \left(\int_{\Omega_I} \mu \boldsymbol{\rho}_k \cdot \boldsymbol{\rho}_l \right). \end{aligned}$$

Hence the voltage equation (4.30) becomes the system

$$\begin{aligned} \sum_{k=1}^M \left(\int_{\Omega_I} \mu \boldsymbol{\rho}_k \cdot \boldsymbol{\rho}_l \right) \frac{dI_k^0}{dt} + \int_{\Gamma} \sigma^{-1} \text{curl } \mathbf{H}_C \cdot (\boldsymbol{\rho}_l \times \mathbf{n}_I) \\ = -(V_l - V_E) + \int_{\Gamma} \sigma^{-1} \mathbf{J}_C \cdot (\boldsymbol{\rho}_l \times \mathbf{n}_I) \quad \text{in } (0, T), \end{aligned} \quad (4.39)$$

for each $l = 1, \dots, M$, where the M voltage jumps $(V_l - V_E)(t)$ have been assigned.

A similar argument can be applied when the conductor Ω_C is the (disjoint) union of $M \geq 2$ connected components $\Omega_{C,k}$, $k = 1, \dots, M$, each one having two electric ports $\Gamma_{E,k}$ and $\Gamma_{J,k}$ (see Figure 3).

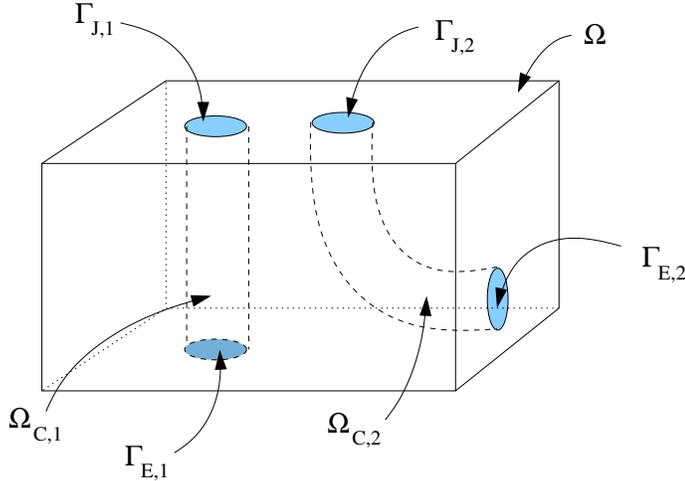


Figure 3: A second alternative geometrical configuration: a non-connected conductor Ω_C with four electric ports.

In this geometrical situation, we have to assign M voltage jumps $(V_{J,k} - V_{E,k})(t)$, $k = 1, \dots, M$, and the dimension of the space \mathcal{H}_I^μ is

still equal to M . Denoting by $\boldsymbol{\rho}_l$ the basis function with the property that $\oint_{\partial^+\Gamma_{J,k}} \boldsymbol{\rho}_l \cdot \boldsymbol{\tau}_{J,k}^+ = \delta_{lk}$, $l = 1, \dots, M$, in this case the voltage system becomes

$$\begin{aligned} \sum_{k=1}^M \left(\int_{\Omega_I} \mu \boldsymbol{\rho}_k \cdot \boldsymbol{\rho}_l \right) \frac{dI_k^0}{dt} + \int_{\Gamma} \sigma^{-1} \operatorname{curl} \mathbf{H}_C \cdot (\boldsymbol{\rho}_l \times \mathbf{n}_I) \\ = -(V_{J,l} - V_{E,l}) + \int_{\Gamma} \sigma^{-1} \mathbf{J}_C \cdot (\boldsymbol{\rho}_l \times \mathbf{n}_I) \quad \text{in } (0, T), \end{aligned} \quad (4.40)$$

for each $l = 1, \dots, M$.

One can also consider the following geometrical situation. The conductor is composed by two connected components: one, denoted by $\Omega_C^{(1)}$, is like the conductor in Section 1, and is a simply-connected domain not strictly contained in Ω . This means that it has an intersection with $\partial\Omega$, denoted by $\partial\Omega_C^{(1)} \cap \partial\Omega = \Gamma_E \cup \Gamma_J$, where Γ_E and Γ_J are two disjoint and connected ‘electric ports’ on $\partial\Omega$. We also suppose that the intersection of $\partial\Omega_C^{(1)}$ and $\partial\Omega$ is transversal. The other connected component $\Omega_C^{(2)}$ is like a hollow cylinder (namely, a torus), and is strictly contained in Ω . One can think of $\Omega_C^{(1)}$ as an induction coil that envelops the workpiece $\Omega_C^{(2)}$, without touching it (see Figure 4).

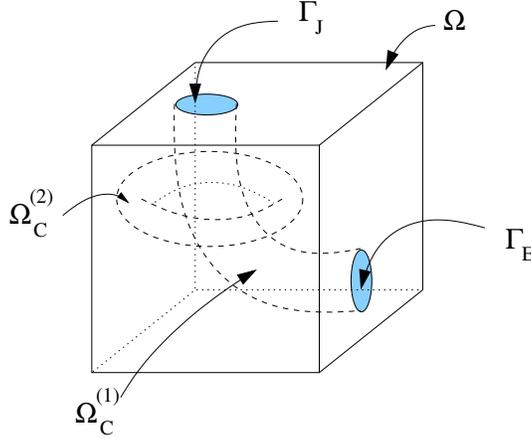


Figure 4: A third alternative geometrical configuration: a non-connected conductor Ω_C with two electric ports.

In this situation, one can identify two non-bounding cycles in Ω_I : the first one, as in the previous cases, is $\sigma^{(1)} = \partial^+\Gamma_J$. The other one is $\sigma^{(2)}$, a cycle linking the hollow cylinder $\Omega_C^{(2)}$, passing into its hole.

Therefore, the dimension of \mathcal{H}_I^μ is equal to 2. Let us choose a basis of \mathcal{H}_I^μ . First we fix an orientation on $\sigma^{(2)}$; then one basis field $\boldsymbol{\rho}_1$ satisfies $\oint_{\partial+\Gamma_J} \boldsymbol{\rho}_1 \cdot \boldsymbol{\tau}_J^+ = 1$ and $\oint_{\sigma^{(2)}} \boldsymbol{\rho}_1 \cdot \boldsymbol{\tau} = 0$, whereas the other basis field $\boldsymbol{\rho}_2$ satisfies $\oint_{\partial+\Gamma_J} \boldsymbol{\rho}_2 \cdot \boldsymbol{\tau}_J^+ = 0$ and $\oint_{\sigma^{(2)}} \boldsymbol{\rho}_2 \cdot \boldsymbol{\tau} = 1$. It is readily seen that the voltage system now is given by

$$\begin{aligned} \sum_{k=1}^2 \left(\int_{\Omega_I} \mu \boldsymbol{\rho}_k \cdot \boldsymbol{\rho}_l \right) \frac{dI_k^0}{dt} + \int_{\Gamma} \sigma^{-1} \operatorname{curl} \mathbf{H}_C \cdot (\boldsymbol{\rho}_l \times \mathbf{n}_I) \\ = -(V_J - V_E) \delta_{l1} + \int_{\Gamma} \sigma^{-1} \mathbf{J}_C \cdot (\boldsymbol{\rho}_l \times \mathbf{n}_I) \quad \text{in } (0, T), \end{aligned} \quad (4.41)$$

for each $l = 1, 2$. Note that this example clearly shows that voltage drops cannot be imposed if the conducting domain Ω_C is strictly contained in Ω and does not have electric ports (in that case, $\boldsymbol{\rho}_1$ does not exist and (4.41) simply becomes an equation for $\boldsymbol{\rho}_2$, in which the first term at the right end side disappears).

5 The optimal control problem

In the previous sections, we prepared the analysis of our state equation, i.e., our Maxwell control system. Now we take the voltage $V_J - V_E$ as control function. For this reason, we set $V(t) = V_J(t) - V_E(t)$. Thanks to Theorem 3.1 we know that (for fixed and given current density \mathbf{J}_C and initial function \mathbf{H}_0) to each function V a unique magnetic field \mathbf{H} in Ω and a unique electric field \mathbf{E}_C in Ω_C are associated. Let us denote these fields by \mathbf{H}_V and $\mathbf{E}_{C,V}$, respectively, to indicate their correspondence to the given voltage V . The control-to-state mapping $V \mapsto (\mathbf{H}_V, \mathbf{E}_{C,V})$ is affine between the corresponding spaces. By (3.20), it is also continuous.

The main goal of the control is to approach given state functions $\mathbf{H}_d \in L^2$ (desired magnetic field) and $\mathbf{E}_{C,d} \in L^2$ (desired electric field) in the associated L^2 -norms, while the ‘‘cost’’ for the electrical voltage V is considered by a Tikhonov regularization term with weight $\nu \geq 0$. This leads to minimizing the following objective functional,

$$\begin{aligned} F(V) := \frac{\nu_H}{2} \int_0^T \|\mathbf{H}_V - \mathbf{H}_d\|_{\mu, \Omega}^2 \\ + \frac{\nu_E}{2} \int_0^T \|\mathbf{E}_{C,V} - \mathbf{E}_{C,d}\|_{\sigma, \Omega_C}^2 + \frac{\nu}{2} \int_0^T |V|^2. \end{aligned} \quad (5.42)$$

The electric field $\mathbf{E}_{C,V}$ is equal to $\mathbf{E}_{C,V} = \sigma^{-1}(\text{curl } \mathbf{H}_{V,C} - \mathbf{J}_C)$, hence we can express the objective functional entirely in terms of the magnetic field,

$$F(V) = \frac{\nu_H}{2} \int_0^T \|\mathbf{H}_V - \mathbf{H}_d\|_{\mu,\Omega}^2 + \frac{\nu_E}{2} \int_0^T \|\sigma^{-1}(\text{curl } \mathbf{H}_{V,C} - \mathbf{J}_C) - \mathbf{E}_{C,d}\|_{\sigma,\Omega_C}^2 + \frac{\nu}{2} \int_0^T |V|^2. \quad (5.43)$$

The control functions V may be restricted by the constraint $V \in \mathcal{V}_{ad}$, where \mathcal{V}_{ad} is a non-empty, convex, and closed subset of $L^2(0, T)$. In this way, our optimal control problem admits the following short form:

$$\min_{V \in \mathcal{V}_{ad}} F(V). \quad (5.44)$$

A control $V^* \in \mathcal{V}_{ad}$ is said to be *optimal* if

$$F(V^*) \leq F(V) \quad \forall V \in \mathcal{V}_{ad}.$$

In other words, an optimal control V^* is defined by $F(V^*) = \min_{V \in \mathcal{V}_{ad}} F(V)$.

Theorem 5.1. *If \mathcal{V}_{ad} is bounded or $\nu > 0$, then the optimal control problem (5.44) has at least one optimal control. In the latter case, the optimal control is unique.*

Proof. In view of Theorem 3.1, the control-to-state mapping $V \mapsto (\mathbf{H}_V, \mathbf{E}_V)$ is (affine) and continuous. Therefore, the functional F is weakly lower semicontinuous in $L^2(0, T)$. The set \mathcal{V}_{ad} is convex and closed in $L^2(0, T)$, hence weakly closed. If \mathcal{V}_{ad} is in addition bounded, then \mathcal{V}_{ad} is weakly compact and the result follows in a standard way. If $\nu > 0$, then we can restrict the search for an optimal control to a bounded and weakly closed subset of \mathcal{V}_{ad} and the result follows in the same way. \square

To proceed with necessary optimality conditions, we need the derivative F' of F . The derivative at \widehat{V} in the direction V is given by

$$F'(\widehat{V})V = \nu_H \int_0^T \int_{\Omega} \mu(\mathbf{H}_{\widehat{V}} - \mathbf{H}_d) \cdot \mathbf{H}_V^0 + \nu_E \int_0^T \int_{\Omega_C} (\mathbf{E}_{C,\widehat{V}} - \mathbf{E}_{C,d}) \cdot \text{curl } \mathbf{H}_{V,C}^0 + \nu \int_0^T \widehat{V} V, \quad (5.45)$$

where $\mathbf{H}_{\widehat{V}}$ and $\mathbf{E}_{C,\widehat{V}} = \sigma^{-1}(\text{curl } \mathbf{H}_{\widehat{V}} - \mathbf{J}_C)$ are the states associated to \widehat{V} , with initial datum \mathbf{H}_0 and current density \mathbf{J}_C , while \mathbf{H}_V^0 is the state associated to V , subject to vanishing initial datum and current density equal to zero.

Obviously, the terms

$$\nu_H \int_0^T \int_{\Omega} \mu(\mathbf{H}_{\widehat{V}} - \mathbf{H}_d) \cdot \mathbf{H}_V^0 \quad \text{and} \quad \nu_E \int_0^T \int_{\Omega_C} (\mathbf{E}_{C,\widehat{V}} - \mathbf{E}_{C,d}) \cdot \text{curl } \mathbf{H}_{V,C}^0$$

depend linearly on V . However, V enters in an implicit way via \mathbf{H}_V^0 and $\text{curl } \mathbf{H}_{V,C}^0$.

For finding an explicit expression in terms of V , an adjoint equation is introduced in a standard way. This is based on a duality argument. Later, first-order optimality conditions for an optimal control V^* are based on this approach.

6 The adjoint problem

Let us first define the adjoint equation.

Definition 6.1 (Adjoint equation). *Let $\widehat{V} \in L^2(0, T)$ be a given control with corresponding states $\mathbf{H}_{\widehat{V}}$ and $\mathbf{E}_{C,\widehat{V}}$. Moreover, let $\mathbf{H}_d \in L^2(0, T; L^2(\Omega)^3)$, $\mathbf{E}_{C,d} \in L^2(0, T; L^2(\Omega_C)^3)$ be the given desired states. The problem to find $\mathbf{w} \in L^2(0, T; \mathbf{W}) \cap C^0([0, T]; \mathbf{X})$ with*

$$\begin{aligned} -\frac{d}{dt} \int_{\Omega} \mu \mathbf{w}(t) \cdot \mathbf{h} + \int_{\Omega_C} \sigma^{-1} \text{curl } \mathbf{w}_C(t) \cdot \text{curl } \mathbf{h}_C \\ = \nu_H \int_{\Omega} \mu(\mathbf{H}_{\widehat{V}} - \mathbf{H}_d)(t) \cdot \mathbf{h} + \nu_E \int_{\Omega_C} (\mathbf{E}_{C,\widehat{V}} - \mathbf{E}_{C,d})(t) \cdot \text{curl } \mathbf{h}_C \end{aligned} \quad (6.46)$$

for all $\mathbf{h} \in \mathbf{W}$ and a.a. $t \in (0, T)$, and

$$\mathbf{w}|_{t=T} = 0 \quad \text{in } \Omega \quad (6.47)$$

is called adjoint equation. Its solution \mathbf{w} is said to be the adjoint state associated with $\widehat{V} \in L^2(0, T)$ and denoted by $\mathbf{w}_{\widehat{V}}$.

Since the bilinear forms at the left hand side of (3.18) are symmetric, it is easy to confirm that the adjoint equation has a unique (weak)

solution \mathbf{w} , hence the adjoint state associated with \widehat{V} is uniquely determined. Moreover, the adjoint equation is well-posed. In particular, the mapping $L^2(0, T) \ni \widehat{V} \mapsto \mathbf{w} \in L^2(0, T; \mathbf{W}) \cap C^0([0, T]; \mathbf{X})$ is continuous.

Now we have all prerequisites to formulate optimality conditions.

Theorem 6.2 (Necessary optimality conditions). *Let V^* be an optimal control of problem (5.44) and let \mathbf{H}_{V^*} and \mathbf{E}_{C, V^*} be the associated optimal magnetic and electric fields, respectively. Then the variational inequality*

$$\int_0^T (-I^{0,*} + \nu V^*)(V - V^*) \geq 0 \quad \forall V \in \mathcal{V}_{ad}, \quad (6.48)$$

has to be satisfied, where $I^{0,*}$ is the total current intensity passing at time t through Γ_J in the direction of \mathbf{n}_C that is generated by the adjoint magnetic field \mathbf{w}_{V^*} . It is defined by

$$I^{0,*}(t) := \oint_{\partial^+ \Gamma_J} \mathbf{w}_{V^*, I}(t) \cdot \boldsymbol{\tau}_J^+.$$

Proof. We know that the optimal control V^* must obey the variational inequality $F'(V^*)(V - V^*) \geq 0$ for each $V \in \mathcal{V}_{ad}$. The first two terms at the right hand side of (5.45) with \widehat{V} substituted by V^* and V substituted by $V - V^*$ are

$$\begin{aligned} & \nu_H \int_0^T \int_{\Omega} \mu(\mathbf{H}_{V^*} - \mathbf{H}_d) \cdot (\mathbf{H}_V^0 - \mathbf{H}_{V^*}^0) \\ & + \nu_E \int_0^T \int_{\Omega_C} (\mathbf{E}_{C, V^*} - \mathbf{E}_{C, d}) \cdot \text{curl}(\mathbf{H}_{V, C}^0 - \mathbf{H}_{V^*, C}^0). \end{aligned}$$

Using (6.46) with $\mathbf{h} = \mathbf{H}_V^0 - \mathbf{H}_{V^*}^0$ gives

$$\begin{aligned} & \nu_H \int_0^T \int_{\Omega} \mu(\mathbf{H}_{V^*} - \mathbf{H}_d) \cdot (\mathbf{H}_V^0 - \mathbf{H}_{V^*}^0) \\ & + \nu_E \int_0^T \int_{\Omega_C} (\mathbf{E}_{C, V^*} - \mathbf{E}_{C, d}) \cdot \text{curl}(\mathbf{H}_{V, C}^0 - \mathbf{H}_{V^*, C}^0) \\ & = - \int_0^T \frac{d}{dt} \int_{\Omega} \mu \mathbf{w}_{V^*} \cdot (\mathbf{H}_V^0 - \mathbf{H}_{V^*}^0) \\ & + \int_0^T \int_{\Omega_C} \sigma^{-1} \text{curl} \mathbf{w}_{V^*, C} \cdot \text{curl}(\mathbf{H}_{V, C}^0 - \mathbf{H}_{V^*, C}^0). \end{aligned} \quad (6.49)$$

Due to the fact that $\mathbf{w}_{V^*}|_{t=T} = \mathbf{0}$ and that $(\mathbf{H}_V^0 - \mathbf{H}_{V^*}^0)|_{t=0} = \mathbf{0}$, we have

$$\int_0^T \frac{d}{dt} \int_{\Omega} \mu \mathbf{w}_{V^*} \cdot (\mathbf{H}_V^0 - \mathbf{H}_{V^*}^0) = 0.$$

Hence, by a change of sign in this vanishing term and by taking into account the symmetry of the bilinear forms, equation (6.49) can be rewritten as

$$\begin{aligned} & \nu_H \int_0^T \int_{\Omega} \mu (\mathbf{H}_{V^*} - \mathbf{H}_d) \cdot (\mathbf{H}_V^0 - \mathbf{H}_{V^*}^0) \\ & \quad + \nu_E \int_0^T \int_{\Omega_C} (\mathbf{E}_{C,V^*} - \mathbf{E}_{C,d}) \cdot \text{curl}(\mathbf{H}_{V,C}^0 - \mathbf{H}_{V^*,C}^0) \\ & = \int_0^T \frac{d}{dt} \int_{\Omega} \mu (\mathbf{H}_V^0 - \mathbf{H}_{V^*}^0) \cdot \mathbf{w}_{V^*} \\ & \quad + \int_0^T \int_{\Omega_C} \sigma^{-1} \text{curl}(\mathbf{H}_{V,C}^0 - \mathbf{H}_{V^*,C}^0) \cdot \text{curl} \mathbf{w}_{V^*,C} \\ & = - \int_0^T (V - V^*) \int_{\Gamma_J} \text{curl} \mathbf{w}_{V^*,C} \cdot \mathbf{n}_C, \end{aligned}$$

having used (3.18) in the final equality. On the other hand, from the Stokes theorem and the matching condition $\mathbf{w}_{V^*,C} \times \mathbf{n}_C = -\mathbf{w}_{V^*,I} \times \mathbf{n}_I$, as in the proof of (4.32) we find

$$\int_{\Gamma_J} \text{curl} \mathbf{w}_{V^*,C} \cdot \mathbf{n}_C = \oint_{\partial^+ \Gamma_J} \mathbf{w}_{V^*,C} \cdot \boldsymbol{\tau}_J^+ = \oint_{\partial^+ \Gamma_J} \mathbf{w}_{V^*,I} \cdot \boldsymbol{\tau}_J^+ = I^{0,*},$$

and the result easily follows. \square

7 Some remarks on numerical approximation

In this section we only present how finite elements could be used for the space discretization of the state and the adjoint problems. A more detailed analysis will be the subject of a further research.

It is clear that an advantage of the proposed formulation (3.18) is that the magnetic field \mathbf{H} is looked for in the space \mathbf{W} , whose elements \mathbf{w} have to satisfy the constraint $\text{curl} \mathbf{w}_I = \mathbf{0}$ in Ω_I . Therefore, the number of degrees of freedom that are needed for the numerical approximation in Ω_I is less than that necessary for a standard approximation of $H(\text{curl}; \Omega_I)$.

In other words, we know that in Ω_I we have $\mathbf{H}_I = \text{grad } \psi_I + \Gamma^0 \boldsymbol{\rho}$, and it is natural to discretize this vector field by employing as degrees of freedom the nodal values of an approximation of the magnetic potential ψ_I (plus the coefficient I^0).

However, the explicit introduction of the magnetic potential ψ_I is not required (in this sense, our method is simpler than that proposed in [5]). In fact, it is much straightforward to furnish a discretization of \mathbf{W} by introducing a suitable finite dimensional subspace $\mathbf{W}_h \subset \mathbf{W}$. This can be easily done: let us give the description of all the basis functions of \mathbf{W}_h .

Let us denote by N_h the space of Nédélec finite elements of the lowest order, and by L_h the space of piecewise-linear, globally continuous Lagrange elements (see, e.g., [19, Chap. 5]). As it is well-known, the degrees of freedom of N_h are given by the line integral over the edges of the mesh, whereas the degrees of freedom of L_h are expressed by the nodal values.

The basis of \mathbf{W}_h is constructed in this way: for all the edges in $\overline{\Omega_C}$ that have at most one endpoint on Γ we select the Nédélec basis function associated to that edge; for all the nodes that are in $\overline{\Omega_I}$, except one, we select the gradient of the Lagrange basis function associated to that node; for the non-bounding cycle in $\overline{\Omega_I}$ we choose a curl free Nédélec element with line integral equal to 1 on that cycle (in a more general geometrical situation, this must be repeated for all the non-bounding cycles in $\overline{\Omega_I}$). In [1, Theor. 3] and [2, Theor. 1] it is proved that this is a basis of \mathbf{W}_h .

A few additional words could be addressed to the way in which the curl free Nédélec element with line integral equal to 1 on the non-bounding cycle is constructed. In [1] it is shown how this can be done, in any geometrical configuration, by means of an automatic procedure that only needs the knowledge of the mesh of the domain. However, in many cases the construction is more direct and, in fact, simpler: it is enough to identify a surface Σ which ‘cuts’ the non-bounding cycle, and ‘double’ the nodes of the mesh on it. In this way the surface has two sides, and the vector field we need is the gradient of the piecewise-linear Lagrange interpolant taking value 1 on all the nodes on one side of Σ , and value 0 on all the other nodes, including those on the other side of Σ .

The spatial discretization of the state problem (3.18) is simply

$$\begin{aligned} \frac{d}{dt} \int_{\Omega} \mu \mathbf{H}_h \cdot \mathbf{w}_h + \int_{\Omega_C} \sigma^{-1} \operatorname{curl} \mathbf{H}_{h,C} \cdot \operatorname{curl} \mathbf{w}_{h,C} \\ = \int_{\Omega_C} \sigma^{-1} \mathbf{J}_C \cdot \operatorname{curl} \mathbf{w}_{h,C} - (V_J - V_E) \int_{\Gamma_J} \operatorname{curl} \mathbf{w}_{h,C} \cdot \mathbf{n}_C, \end{aligned} \quad (7.50)$$

for all $\mathbf{w}_h \in \mathbf{W}_h$ and for almost all $t \in (0, T)$. A similar discretization can be devised for the adjoint problem (6.46).

We can thus conclude that, with respect to other formulations of the eddy current problem (say, in terms of the electric field \mathbf{E} , or of the magnetic vector potential \mathbf{A} satisfying $\operatorname{curl} \mathbf{A} = \mu \mathbf{H}$), the one we propose is the cheapest one with respect to the total number of degrees of freedom. Moreover, the algebraic structure of the finite element stiffness matrix is quite favorable, as it is symmetric and positive semi-definite; consequently, any implicit time-discretization scheme will lead at each time step to the solution of an algebraic linear system associated to a sparse, symmetric and positive definite matrix.

Acknowledgments

The authors are warmly grateful to Ana Alonso Rodríguez for having provided them with the pictures.

References

- [1] A. Alonso Rodríguez, E. Bertolazzi, R. Ghiloni, and A. Valli, Construction of a finite element basis of the first de Rham cohomology group and numerical solution of 3D magnetostatic problems. *SIAM J. Numer. Anal.*, **51** (2013), 2380–2402.
- [2] A. Alonso Rodríguez, E. Bertolazzi, R. Ghiloni, and A. Valli, Finite element simulation of eddy current problems using magnetic scalar potentials. *J. Comput. Phys.*, **294** (2015), 503–523.
- [3] A. Alonso Rodríguez and A. Valli, *Eddy current approximation of Maxwell equations*. Springer-Verlag Italia, Milan, 2010.

- [4] L. Arnold and B. von Harrach, A unified variational formulation for the parabolic-elliptic eddy current equations. *SIAM J. Appl. Math.*, **72** (2012), 558–576.
- [5] A. Bermudez, B. López Rodríguez, R. Rodríguez, and P. Salgado, Numerical solution of transient eddy current problems with input current intensities as boundary data. *IMA J. Numer. Anal.*, **32** (2012), 1001–1029.
- [6] V. Bommer and I. Yousept. Optimal control of the full time-dependent Maxwell equations, *ESAIM Math. Model. Numer. Anal.*, **50** (2016), 237–261.
- [7] A. Bossavit. Most general ‘non-local’ boundary conditions for the Maxwell equations in a bounded region, *COMPEL*, **19** (2000), 239–245.
- [8] R. Dautray and J.-L. Lions, *Mathematical analysis and numerical methods for science and technology. Vol. 5*. Springer-Verlag, Berlin, 1992.
- [9] P.E. Druet, O. Klein, J. Sprekels, F. Tröltzsch, and I. Yousept, Optimal control of three-dimensional state-constrained induction heating problems with nonlocal radiation effects. *SIAM J. Control Optim.*, **49** (2011), 1707–1736.
- [10] R. Griesse and K. Kunisch, Optimal control for a stationary MHD system in velocity-current formulation. *SIAM J. Control Optim.*, **45** (2006), 1822–1845.
- [11] M. Gunzburger and C. Trenchea, Analysis and discretization of an optimal control problem for the time-periodic MHD equations. *J. Math. Anal. Appl.*, **308** (2005), 440–466.
- [12] M. Hinze, Control of weakly conductive fluids by near wall Lorentz forces. *GAMM-Mitt.*, **30** (2007), 149–158.
- [13] D. Hömberg and J. Sokołowski, Optimal shape design of inductor coils for surface hardening. *Numer. Funct. Anal. Optim.*, **42** (2003), 1087–1117.
- [14] D. Hömberg and S. Volkwein, Control of laser surface hardening by a reduced-order approach using proper orthogonal decomposition. *Math. Comput. Modelling*, **38** (2003), 1003–1028.

- [15] L. S. Hou and A. J. Meir, Boundary optimal control of MHD flows. *Appl. Math. Optim.*, **32** (1995), 143–162.
- [16] L. S. Hou and S. S. Ravindran, Computations of boundary optimal control problems for an electrically conducting fluid. *J. Comput. Phys.*, **128** (1996), 319–330.
- [17] M. Kolmbauer, *The multiharmonic finite element and boundary element method for simulation and control of eddy current problems*. Ph.D thesis, Johannes Kepler University Linz, 2012.
- [18] M. Kolmbauer and U. Langer, A robust preconditioned MinRes solver for distributed time-periodic eddy current optimal control problems. *SIAM J. Sci. Comput.*, **34** (2012), B785–B809.
- [19] P. Monk, *Finite element methods for Maxwell’s equations*. Oxford University Press, New York, 2003.
- [20] S. Nicaise, S. Stingelin, and F. Tröltzsch, On two optimal control problems for magnetic fields. *Comput. Methods Appl. Math.*, **14** (2014), 555–573.
- [21] S. Nicaise, S. Stingelin, and F. Tröltzsch, Optimal control of magnetic fields in flow measurement. *Discrete Contin. Dyn. Syst. Ser. S*, **8** (2015), 579–605.
- [22] S. Nicaise and F. Tröltzsch, Optimal control of some quasilinear Maxwell equations of parabolic type. *Discrete Contin. Dyn. Syst. Ser. S*, **10** (2017), 1375–1391.
- [23] S. S. Ravindran, Real-time computational algorithm for optimal control of an MHD flow system. *SIAM J. Sci. Comput.*, **26** (2005), 1369–1388.
- [24] F. Tröltzsch and A. Valli, Modeling and control of low-frequency electromagnetic fields in multiply connected conductors. In *System Modeling and Optimization* (eds. L. Bociu, J.-A. Desideri, and A. Habbal), Springer, (2017), 505–516.
- [25] F. Tröltzsch and A. Valli, Optimal control of low-frequency electromagnetic fields in multiply connected conductors. *Optimization*, **65** (2016), 1651–1673.
- [26] I. Yousept, Optimal control of Maxwell’s equations with regularized state constraints. *Comput. Optim. Appl.*, **52** (2012), 559–581.

- [27] I. Yousept, Optimal bilinear control of eddy current equations with grad-div regularization. *J. Numer. Math.*, **23** (2015), 81–98.
- [28] I. Yousept and F. Tröltzsch, PDE-constrained optimization of time-dependent 3D electromagnetic induction heating by alternating voltages. *ESAIM Math. Model. Numer. Anal.*, **46** (2012), 709–729.